

HW 6

§ 6.5

(20)

$$\begin{aligned}
 x &= \sqrt{2y-1}, \quad \frac{5}{8} \leq y \leq 1; \quad y\text{-axis} \\
 S &= \int_{5/8}^1 2\pi x \sqrt{1 + \left(\frac{1}{\sqrt{2y-1}}\right)^2} dy \\
 &= 2\pi \int_{5/8}^1 \sqrt{2y-1} \cdot \sqrt{\frac{2y-1}{2y-1} + \frac{1}{2y-1}} dy \\
 &= 2\pi \int_{5/8}^1 \sqrt{2y} dy \\
 &= 2\sqrt{2}\pi \left(\frac{2}{3} y^{3/2} \Big|_{5/8}^1 \right) = 2\sqrt{2}\pi \left(\frac{2}{3}(1) - \frac{2}{3}\left(\frac{5\sqrt{5}}{16\sqrt{2}}\right) \right) \\
 &= \boxed{\frac{4}{3}\sqrt{2}\pi \left(1 - \frac{5\sqrt{5}}{16\sqrt{2}}\right)}
 \end{aligned}$$

(24)

$$\begin{aligned}
 y &= \cos x, \quad -\frac{\pi}{2} \leq x \leq \frac{\pi}{2}; \quad x\text{-axis} \\
 S &= \int_{-\pi/2}^{\pi/2} 2\pi y \sqrt{1 + \sin^2 x} dx \\
 &= \int_{-\pi/2}^{\pi/2} 2\pi (\cos x) \sqrt{1 + \sin^2 x} dx \\
 S &= \boxed{2\pi \int_{-\pi/2}^{\pi/2} (\cos x) \sqrt{1 + \sin^2 x} dx}
 \end{aligned}$$

(28)

$$\begin{aligned}
 S &= 2\pi \int_a^{ah} y \cdot \sqrt{1 + \left(\frac{-x}{\sqrt{r^2-x^2}}\right)^2} dx \\
 &= 2\pi \int_a^{ah} \sqrt{r^2-x^2} \sqrt{1 + \frac{x^2}{r^2-x^2}} dx \\
 &= 2\pi \int_a^{ah} \sqrt{r^2-x^2+x^2} dx = 2\pi \int_a^{ah} r dx \\
 S &= \boxed{2\pi r h} \quad (\text{independent of } a)
 \end{aligned}$$

(30)

$$\begin{aligned}
 \text{a) } x^2 + y^2 &= 45^2 \Rightarrow x = \sqrt{45^2 - y^2} \Rightarrow \frac{dx}{dy} = \frac{-y}{\sqrt{45^2 - y^2}} \\
 S &= 2\pi \int_{-22.5}^{45} \sqrt{45^2 - y^2} \cdot \sqrt{1 + \frac{y^2}{45^2 - y^2}} dy \\
 &= 2\pi \int_{-22.5}^{45} 45 dy \\
 &= 2\pi (45)(45 + 22.5) = \boxed{6075 \pi \text{ ft}^2} \\
 \text{b) } 6075 (3.1415) &= 19084.6 \approx \boxed{19,085 \text{ ft}^2}
 \end{aligned}$$

$$\begin{aligned}
 (32) \quad x^{2/3} + y^{2/3} = 1 &\Rightarrow y = (1 - x^{2/3})^{3/2} \Rightarrow \frac{dy}{dx} = \frac{3}{2} \cdot \left(\frac{2}{3}\right) x^{-1/3} \sqrt{1 - x^{2/3}} \\
 S &= 2 \cdot 2\pi \int_0^1 (1 - x^{2/3})^{3/2} \cdot \sqrt{1 + \frac{1 - x^{2/3}}{x^{2/3}}} dx \\
 &= 4\pi \int_0^1 (1 - x^{2/3})^{3/2} \sqrt{\frac{1}{x^{2/3}}} dx \\
 &= 4\pi \int_0^1 (1 - x^{2/3})^{3/2} \cdot x^{-1/3} dx \\
 & \left[\text{Let } u = 1 - x^{2/3} \Rightarrow du = -\frac{2}{3} x^{-1/3} dx \right] \\
 S &= -6\pi \int_0^1 u^{3/2} du = -6\pi \left(\frac{2}{5} u^{5/2} \Big|_0^1 \right) \\
 &= -6\pi \left[\frac{2}{5} (1 - x^{2/3})^{5/2} \Big|_0^1 \right] = -6\pi \left[\frac{2}{5} (0) - \frac{2}{5} (1) \right] \\
 \boxed{S} &= \frac{12\pi}{5}
 \end{aligned}$$

$$\begin{aligned}
 (36) \quad x &= a(t - \sin t), \quad y = a(1 - \cos t), \quad 0 \leq t \leq 2\pi; \quad x\text{-axis} \\
 \frac{dx}{dt} &= a(1 - \cos t), \quad \frac{dy}{dt} = a(\sin t) \\
 S &= 2\pi \int_0^{2\pi} a(1 - \cos t) \sqrt{a^2(1 - 2\cos t + \cos^2 t) + a^2 \sin^2 t} dt \\
 &= 2\pi \int_0^{2\pi} a(1 - \cos t) \sqrt{a^2 - 2a^2 \cos t + a^2} dt \\
 &= 2\pi \int_0^{2\pi} a(1 - \cos t) \cdot a\sqrt{2} \sqrt{1 - \cos t} dt \\
 \boxed{S} &= 2\pi a^2 \sqrt{2} \int_0^{2\pi} (1 - \cos t)^{3/2} dt
 \end{aligned}$$

$$\begin{aligned}
 (42) \quad S &= \int_a^b 2\pi f(x) dx \quad (\text{Eqn. 8}) \\
 &= \int_0^{\sqrt{3}} 2\pi \left(\frac{x}{\sqrt{3}}\right) dx \\
 &= \frac{2\pi}{\sqrt{3}} \left(\frac{1}{2} x^2 \Big|_0^{\sqrt{3}} \right) = \frac{2\pi}{\sqrt{3}} \cdot \frac{1}{2} (3 - 0) \\
 &= \frac{3\pi}{\sqrt{3}} = \boxed{\sqrt{3} \pi}
 \end{aligned}$$

$$\begin{aligned}
 (48) \quad S &= 2\pi \rho L \Rightarrow 2\pi \left(a - \frac{2a}{\pi} \right) (\pi a) \\
 &= 2\pi^2 a \left(\frac{\pi a - 2a}{\pi} \right) = \boxed{2\pi a^2 (\pi - 2)}
 \end{aligned}$$

52) Line \perp to $y = x - a$ and passing through $(0, \frac{2a}{\pi})$ is $y = -x + \frac{2a}{\pi}$.

Intersection of these two lines is where

$$x - a = -x + \frac{2a}{\pi} \Rightarrow 2x = \frac{2a}{\pi} + \frac{\pi a}{\pi}$$

$$\Rightarrow x = \frac{a(2 + \pi)}{2\pi}$$

$$\Rightarrow y = -\left(\frac{2a + a\pi}{2\pi}\right) + \frac{2a}{\pi} = \frac{2a - a\pi}{2\pi}$$

So distance from centroid to axis of rotation is

$$d = \sqrt{\left(\frac{a(2 + \pi)}{2\pi}\right)^2 + \left(\frac{2a - a\pi}{2\pi} - \frac{2a}{\pi}\right)^2}$$

$$= \sqrt{\frac{a^2(4 + 4\pi + \pi^2)}{4\pi^2} + \left(\frac{-2a - a\pi}{2\pi}\right)^2}$$

$$= \sqrt{\frac{4a^2 + 4a^2\pi + a^2\pi^2 + 4a^2 + 4\pi a^2 + a^2\pi^2}{4\pi^2}}$$

$$= \sqrt{\frac{8a^2 + 8a^2\pi + 2a^2\pi^2}{4\pi^2}}$$

$$= \frac{a}{2\pi} \sqrt{8 + 8\pi + 2\pi^2} = \frac{a\sqrt{2}}{2\pi} \sqrt{\pi^2 + 4\pi + 4} = \frac{a\sqrt{2}}{2\pi} (\pi + 2)$$

$$\text{So } S = 2\pi\rho L$$

$$= 2\pi \cdot \frac{a\sqrt{2}}{2\pi} (\pi + 2) (\pi a)$$

$$S = a^2\pi\sqrt{2}(\pi + 2)$$

§ 6.6

④ $F = kx$, so $90 \text{ N} = k(1 \text{ m}) \Rightarrow k = 90 \frac{\text{N}}{\text{m}}$.

Then $W = \int_0^5 kx \, dx = 90 \int_0^5 x \, dx = \frac{90}{2} (25) = \boxed{1125 \text{ J}}$

⑪ Force against the piston is $F = pA$.

$V = Ax$, where x is ht. of the cylinder, then

$$dV = A \, dx.$$

$$\Rightarrow W = \int F \, dx = \int pA \, dx = \int_{(p_1, V_1)}^{(p_2, V_2)} p \, dV.$$

⑫ $pV^{1.4} = c \Rightarrow p = cV^{-1.4}$

So $V_1 = 243 \text{ in}^3$, $p_1 = 50 \text{ lb/in}^3 \Rightarrow c = 50(243)^{1.4} = 109,350 \text{ lb}$.

$$\begin{aligned} \text{So } W &= \int_{243}^{32} (109,350) V^{-1.4} \, dV \\ &= \frac{109,350}{-0.4} \cdot V^{-0.4} \Big|_{243}^{32} = \boxed{-37,968.75 \text{ in} \cdot \text{lb}} \end{aligned}$$

⑬ Let $r =$ constant rate of leakage.

Since bucket is leaking at constant rate and being lifted at a constant rate, then

amt. of H_2O in bucket is proportional to

$(20-x)$. (the distance the bucket is being raised.)

Leakage rate is $\frac{16 \text{ lbs}}{20 \text{ ft}} = .8 \text{ lb/ft}$ raised and

wt. of H_2O in bucket is $F = .8(20-x)$.

$$\begin{aligned} \text{So } W &= \int_0^{20} .8(20-x) \, dx = 16x - .4x^2 \Big|_0^{20} = 320 - \frac{4}{10}(20^2) \\ &= \boxed{160 \text{ ft} \cdot \text{lb}} \end{aligned}$$

(14) Same conditions as in #13 except leakage rate is $\frac{40 \text{ lbs}}{20 \text{ ft}} = 2 \text{ lb/ft}$ raised.

Wt. of H_2O in bucket is $F = 2(20-x)$, so

$$W = \int_0^{20} 2(20-x) dx = 2 \left(20x - \frac{1}{2}x^2 \Big|_0^{20} \right) \\ = 2(400 - 200) = \boxed{400 \text{ ft}\cdot\text{lb}}$$

(18) Each "slab" of oil is to be pumped to a height of 14 ft. So the work to pump a slab is

$(14-y)(\pi)\left(\frac{y}{2}\right)^2$. Since the tank is half full and $V_{\text{original}} = \frac{1}{3}\pi r^2 h = \frac{1}{3}\pi(5^2)(10) = \frac{250\pi}{3} \text{ ft}^3$, then $V_{\text{half}} = \frac{250\pi}{6} \text{ ft}^3$. With half the volume

the cone is filled to height y

$$\Rightarrow \frac{250\pi}{6} = \frac{1}{3}\pi\left(\frac{y}{2}\right)^2 \cdot y = \frac{\pi}{12}y^3 \Rightarrow y = \sqrt[3]{500} \text{ ft.}$$

$$\text{So } W = \int_0^{\sqrt[3]{500}} \frac{57\pi}{4}(14y^2 - y^3) dy \approx \boxed{60,042 \text{ ft}\cdot\text{lb}}$$

(20) Both methods need to pump H_2O 15 ft to base of tank. Pumping to the rim requires an additional 6 ft (so an avg. of 3 extra ft. to pump to the bottom of the tank).

Force of $H_2O = \text{Wt. of } H_2O \approx 62.4 \text{ lb/ft}^3$

So pumping through the valve uses

$(\sqrt{3} \text{ ft})(4\pi)(6 \text{ ft}^3)(62.4 \text{ lb/ft}^3) \approx 14,115 \text{ ft}\cdot\text{lb}$ less work and thus is faster.

$$(22) \quad y = x^2 \Rightarrow x = \sqrt{y}$$

$$\Delta V = \pi (\text{radius})^2 (\text{thickness}) = \pi (\sqrt{y})^2 \Delta y = \pi y \Delta y$$

$$F(y) = \text{Weight} = 10,000 \frac{\text{N}}{\text{m}^3} \cdot \Delta V = (10,000 \frac{\text{N}}{\text{m}^3}) \pi (y \text{ m}^2) \Delta y \text{ m}$$

$$= 10,000 \pi y \Delta y \text{ N.}$$

Ht of tank is $4^2 = 16 \text{ m}$.

Distance to top of tank: $(16 - y) \text{ m}$, so

$$W = \int_0^{16} 10,000 \pi y (16 - y) dy$$

$$\approx \boxed{21,446,605.9 \text{ J}}$$

§ 6.7

② Plate's right-hand edge given by
 $y = x - 3 \Rightarrow x = y + 3$.

Total width is then $2x = 2(y + 3) = 2y + 6$.

Depth of a strip is $2 - y$, so force of
 H_2O is given by

$$\begin{aligned} F &= \int_{-3}^0 w \cdot (\text{strip depth}) \cdot L(y) \, dy \\ &= \int_{-3}^0 (62.4) (2 - y) (2y + 6) \, dy \\ &= 124.8 \int_{-3}^0 (2 - y)(y + 3) \, dy \\ &= 124.8 \int_{-3}^0 (6 - y^2 - y) \, dy = \boxed{1684.8 \text{ lb}} \end{aligned}$$

⑭ a) $V = (1000 \frac{ft^3}{h})(9h) = 9000 ft^3$

$$V = (\text{area of base})(ht) = (1500 ft^2)h$$

$$\text{So } 9000 ft^3 = (1500 ft^2)h \Rightarrow h = 6 ft.$$

So strip depth is $6 - y$,

Total width is $2x = 2y = L(y)$,

$$\text{So } F = 62.4 \int_0^6 (6 - y)(2y) \, dy = \boxed{332.8 \text{ lb}}$$

b) want to find maximum h so that

$$520 \text{ lb} = 62.4 \int_0^h (h - y)(2y) \, dy$$

$$\Rightarrow 520 \text{ lb} = 124.8 \int_0^h (hy - y^2) \, dy$$

$$\Rightarrow \frac{520}{124.8} = \frac{h}{2} y^2 - \frac{1}{2} y^3 \Big|_0^h = \frac{h}{2} - \frac{1}{3}$$

$$\Rightarrow \boxed{h = 9 ft}$$

(15) Pressure at level y is $p = w \cdot h = w \cdot y$, so
 the avg. pressure $\bar{p} = \frac{1}{b} \int_0^b w y \, dy$
 $= \frac{1}{b} \left(\frac{w}{2} y^2 \Big|_0^b \right) = \frac{1}{b} \cdot \frac{w}{2} \cdot b^2$
 $= \frac{bw}{2}$.

(Note that this is the pressure at level $y = \frac{b}{2}$, which is the middle of the plate).

(16) $F = \int_a^b w(\text{depth})(\text{length}) \, dy = \int_0^b w(y)(a) \, dy$
 $= aw \left(\frac{1}{2} y^2 \Big|_0^b \right) = \frac{awb^2}{2} = \left(\frac{bw}{2} \right) (ab) = \bar{p} \cdot \text{Area}.$

(17) When water reaches the top of the tank, the force on the moving side is

$$F = 62.4 \int_{-2}^0 (2\sqrt{4-y^2})(-y) \, dy = 332.8 \text{ ft} \cdot \text{lb}.$$

The force compressing the spring is $F = 100 \cdot x$, so when the tank is full we have

$$332.8 = 100x \Rightarrow x = 3.328 \text{ ft}.$$

Since $x < 5$, the moveable end will not reach the drain hole and the tank will overflow.

(22) $F = 62.4 \int_0^{24} (24-y) \left(\frac{26}{24} \right) (100) \, dy = \boxed{1,946,880 \text{ lb}}$

(where $\frac{26}{24} \cdot 100 \, \Delta y$ is the area of a strip of height Δy and parallel to the base of the dam).