

Recall curl $\vec{F} = \nabla \times \vec{F}$

where

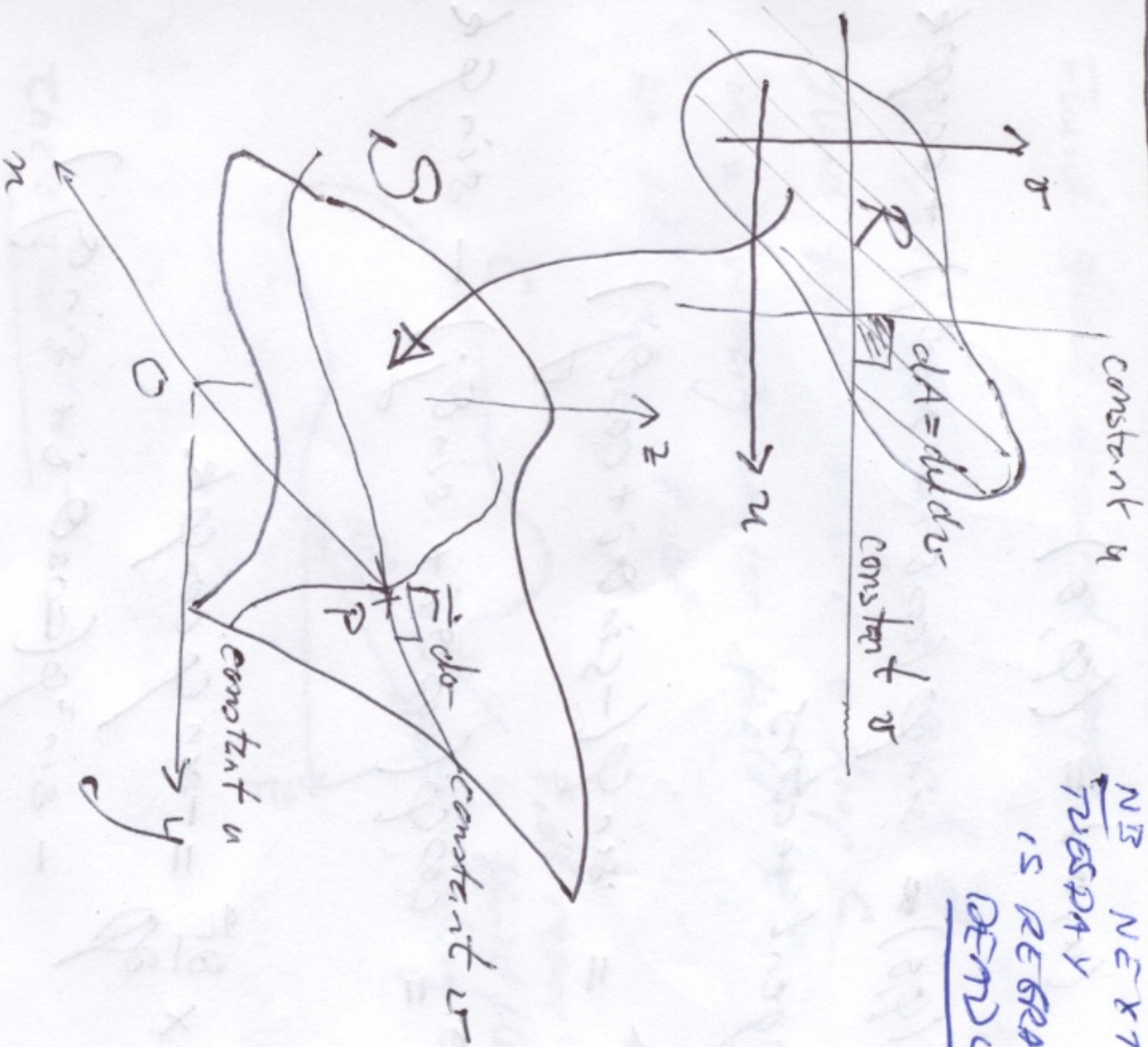
$$\nabla = i \frac{\partial}{\partial x} + j \frac{\partial}{\partial y} + k \frac{\partial}{\partial z}$$

Next time — on example.

Lecture #23 PARAMETERIZED SURFACES

NEXT
TUESDAY

IS REGRAD
DEMDLINE



$$P \in S, \quad \vec{r} = \overrightarrow{OP} = f(u,v)i + g(u,v)j + h(u,v)k$$

Tangent vectors

$$\frac{\partial \vec{r}}{\partial u} = \vec{r}_u$$

$$\frac{\partial \vec{r}}{\partial v} = \vec{r}_v$$

Infinitesimal surface area

$$d\sigma = \left| \frac{\partial \vec{r}}{\partial u} \times \frac{\partial \vec{r}}{\partial v} \right| du dv$$

Example The sphere

$$(u, \sigma) = (\varphi, \theta)$$

$$\vec{r}(\varphi, \theta) = \sin \varphi (\cos \theta \hat{i} + \sin \theta \hat{j}) + \cos \varphi \hat{k}$$

Tangent vectors

$$\frac{\partial \vec{r}}{\partial \theta} = \sin \varphi (-\sin \theta \hat{i} + \cos \theta \hat{j})$$

$$\frac{\partial \vec{r}}{\partial \varphi} = \cos \varphi (\cos \theta \hat{i} + \sin \theta \hat{j}) - \sin \varphi \hat{k}$$

$$\frac{\partial \vec{r}}{\partial \theta} \times \frac{\partial \vec{r}}{\partial \varphi} = -\sin \varphi \cos \varphi \hat{k} - \sin^2 \varphi (\cos \theta \hat{i} + \sin \theta \hat{j})$$

$$\left| \frac{\partial \vec{r}}{\partial \theta} \times \frac{\partial \vec{r}}{\partial \varphi} \right|^2 = \sin^2 \varphi \cos^2 \varphi + \sin^4 \varphi = \sin^2 \varphi$$

$$\Rightarrow d\sigma = \sin \varphi d\varphi d\theta$$

$$\text{SURFACE AREA} = \int d\sigma = \int_0^{2\pi} \int_0^\pi \sin \varphi d\varphi d\theta$$

$$= 2\pi \cdot 2 = 4\pi$$

Recall surface area of radius r sphere = $4\pi r^2$

This answer could not possibly depend on our names for the coordinates & unit vectors $\hat{i}, \hat{j}, \hat{k}$.

The important thing is that $\hat{k}$ is $\vec{n}$, the vector normal to the loop C . For small loops of area $d\sigma$, there is a well-defined normal $\vec{n}$.

then for any loop $C = \partial S$ bounding a surface S

$$\oint_C \vec{F} \cdot d\vec{r} = \int_S d\sigma \underbrace{(\nabla \times \vec{F}) \cdot \vec{n}}_{\text{circulation density}}$$

Add up circulation for small loops

$$\text{Circulation} = \oint_C \vec{F} \cdot d\vec{r} = \int_S \text{curl } \vec{F} \cdot d\vec{A} \quad (\text{circulation density})$$

LINE INTEGRAL

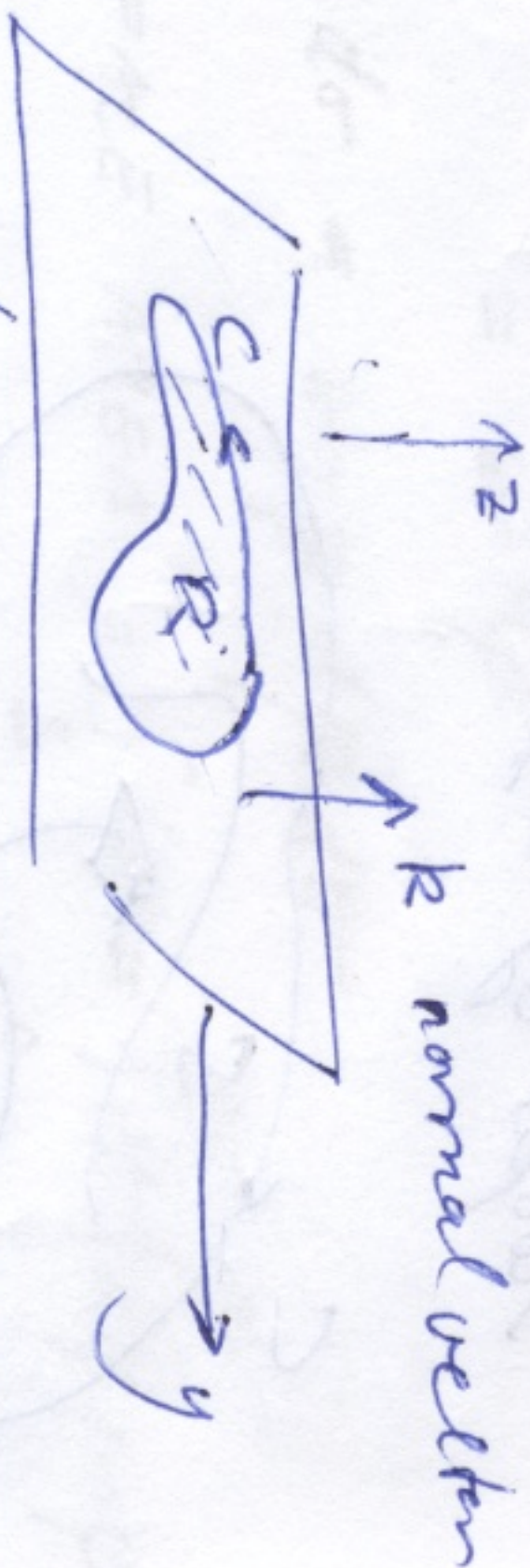
SURFACE INTEGRAL

QUESTION: How do we find circulation density?

ANSWER

For loops in the plane we did it already:

GREEN'S THEOREM (CIRCULATION FORM)



$$\oint_C \vec{F} \cdot d\vec{r} = \int_R \text{curl } \vec{F} \cdot \vec{k} \, dA$$

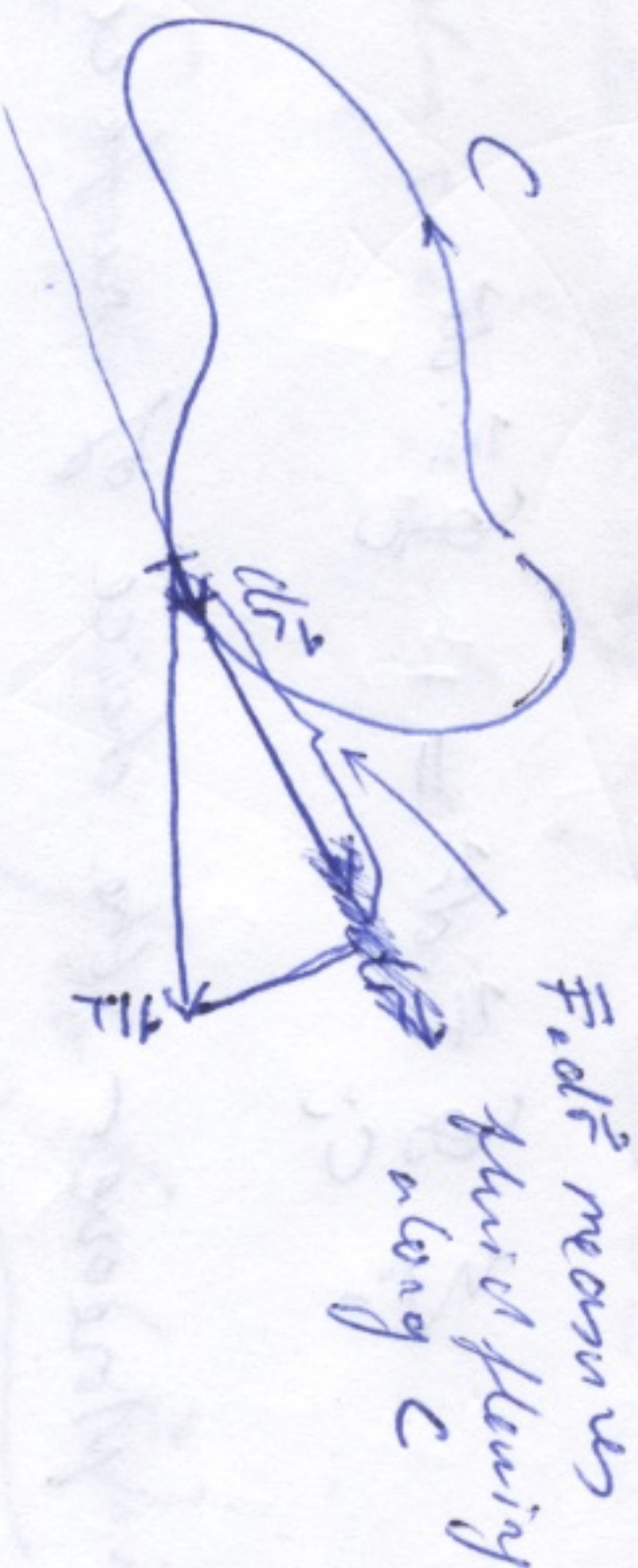
circulation density

STOKES' THEOREM 16.7

Fluid flows around loops

To calculate the amount of fluid flowing around a loop C in a velocity vector field $\vec{F}$

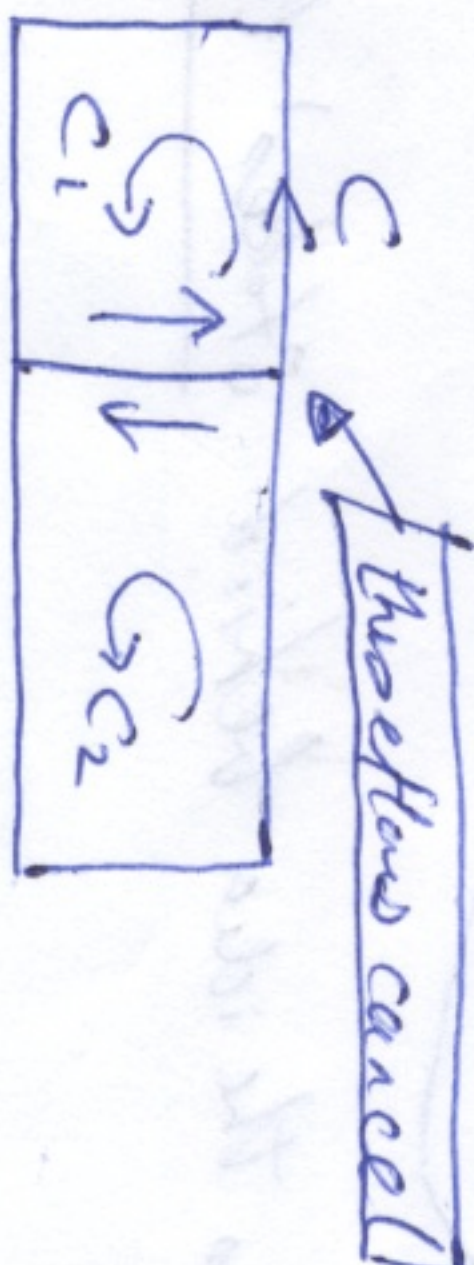
We add up $\vec{F} \cdot d\vec{r}$



The circulation

$$\oint_C \vec{F} \cdot d\vec{r} \text{ measures fluid flowing around } C$$

Consider C built from two loops C_1 & C_2

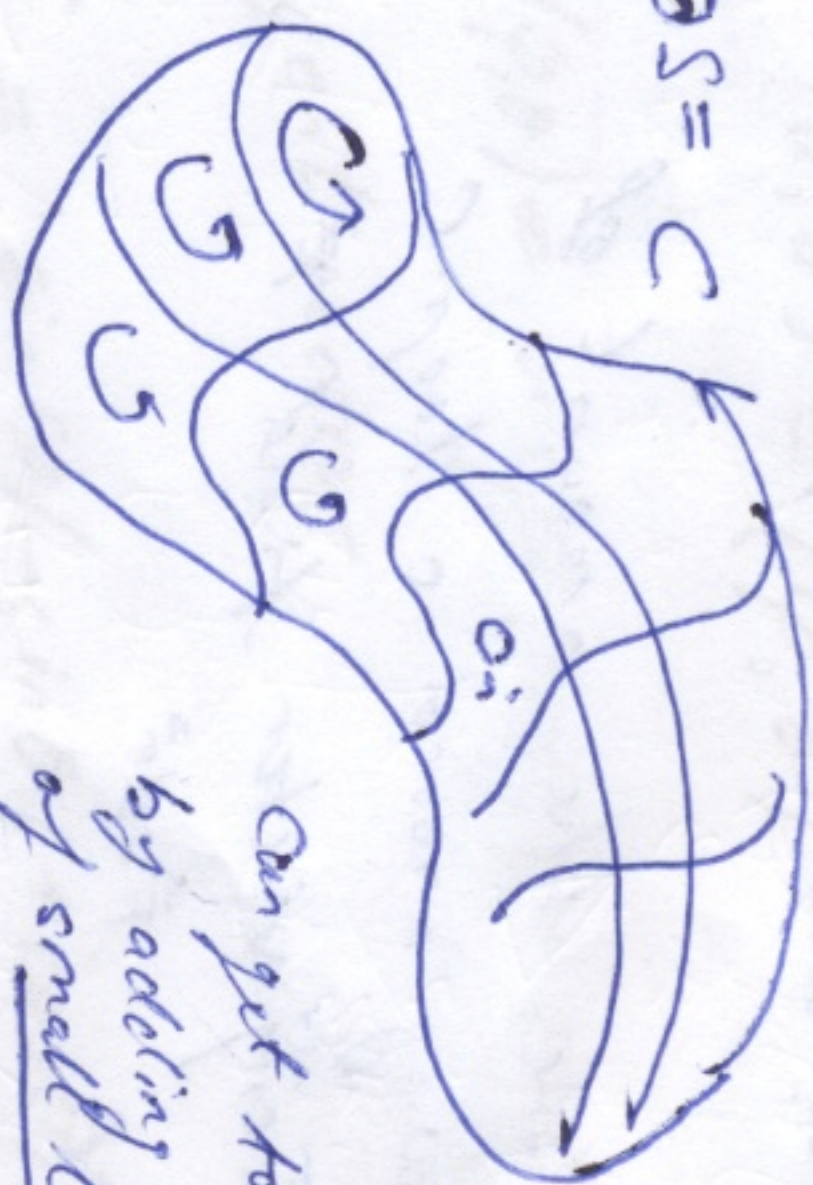


$$\oint_C \vec{F} \cdot d\vec{r} = \oint_{C_1} \vec{F} \cdot d\vec{r} + \oint_{C_2} \vec{F} \cdot d\vec{r}$$

Similarly for

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$$\partial S = C$$



Can get total circulation
by adding circulations
of small loops.

$$\sum_i \oint_{C_i} \vec{F} \cdot d\vec{r} = \oint_C \vec{F} \cdot d\vec{r}$$

Moreover the choice of surface

S shouldn't matter so long as $C = \partial S$



$$C = \partial S$$

This is the idea behind Stokes' theorem.

(i) Start with loop C



(ii) Find some surface S whose

boundary $\partial S = C$

$$\partial S = C$$



(iii) Break S into infinitesimal
loops of size $d\sigma$



(iv) Calculate circulation around
infinitesimal loop

(circulation density) $\times d\sigma$

Depends on $\vec{F}$

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